

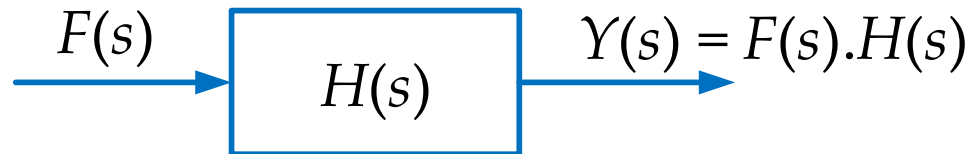
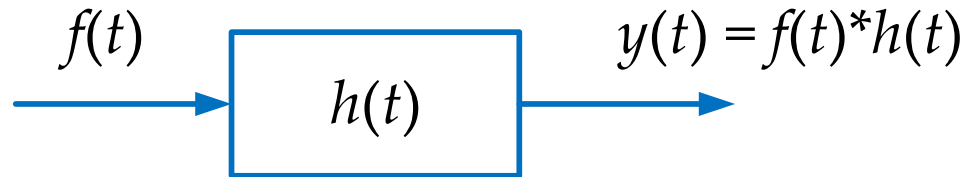
Chapter 5:

System analysis using transfer function

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1. Transfer function
2. Block diagram
3. System described by differential equation
4. System realization
5. Feedback and Control systems

Transfer function:



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- $h(t)$: impulse response of system.

$$H(s) = \text{Laplace transform of } h(t)$$

- **$H(s)$: transfer function**
- Example 5.01: determine transfer function of the system

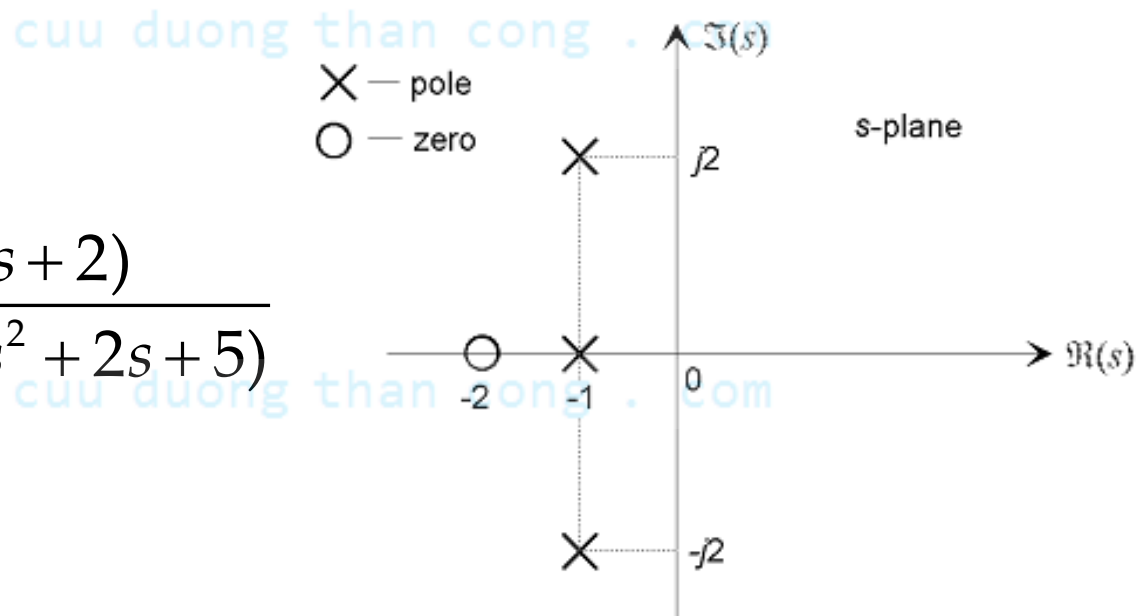
$$y(t) = \int_{-\infty}^t e^{-(t-\tau)} f(\tau) d\tau$$

Zero-pole pattern:

$$H(s) = \frac{P(s)}{Q(s)} = K \frac{(s - z_1) \dots (s - z_m)}{(s - p_1) \dots (s - p_n)}$$

- Zeros (z_i): roots of the equation $P(s) = 0$.
- Poles (p_i): roots of the equation $Q(s) = 0$.
- K : gain constant

$$H(s) = \frac{3(s + 2)}{(s + 1)(s^2 + 2s + 5)}$$



Stability:

- A system is stable when

$$\int_{-\infty}^{\infty} |h(\tau)| d\tau < \infty$$

Quiz 1: stable or unstable?

a. $h(t) = c$ (constant) b. $h(t) = \cos(\omega_0 t + \varphi)$

Quiz 2: stable or unstable?

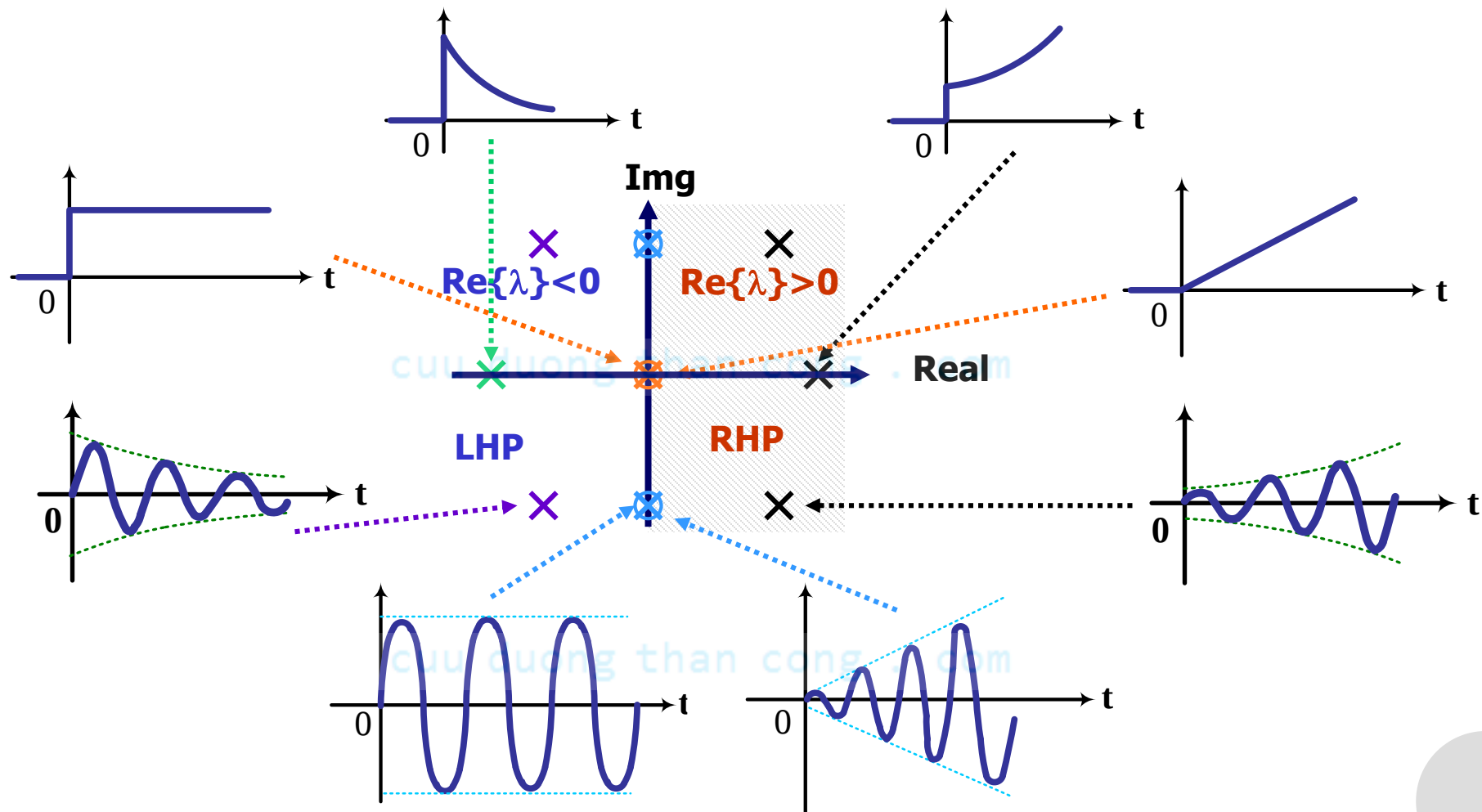
a. $H(s) = \frac{s}{(s+1)(s^2+2s+5)}$

b. $H(s) = \frac{s^2-1}{s(s+1)^2}$

c. $H(s) = \frac{2s+1}{s^2(s^2+4s+5)}$

d. $H(s) = \frac{s^2+s+1}{(s+1)(s+2)(s-3)}$

Stability:



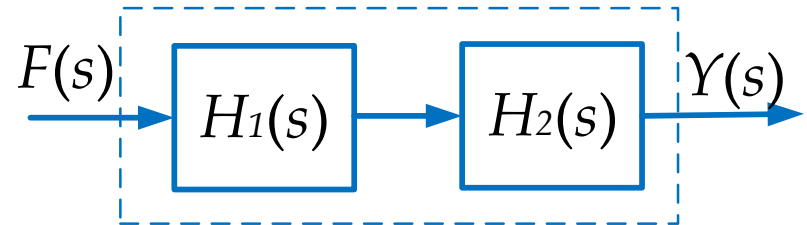
Chapter 5: System analysis using transfer function

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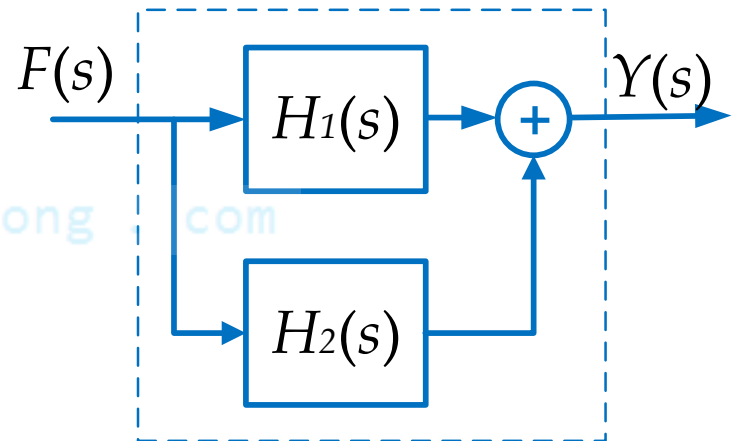
1. Transfer function
2. **Block diagram**
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Block diagram:

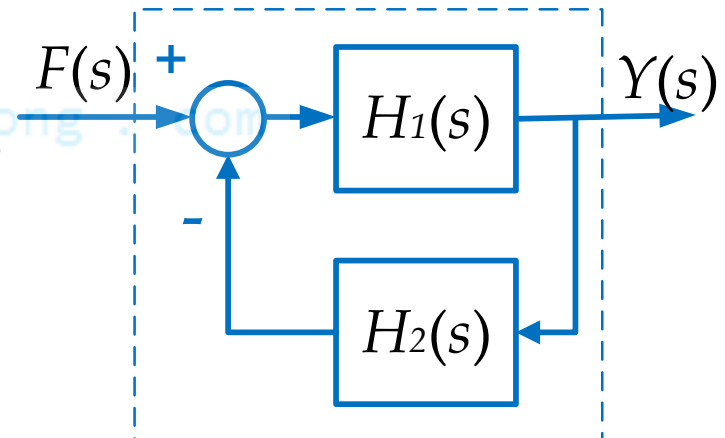
- In series: $H(s) = H_1(s).H_2(s)$



- In parallel: $H(s) = H_1(s) + H_2(s)$

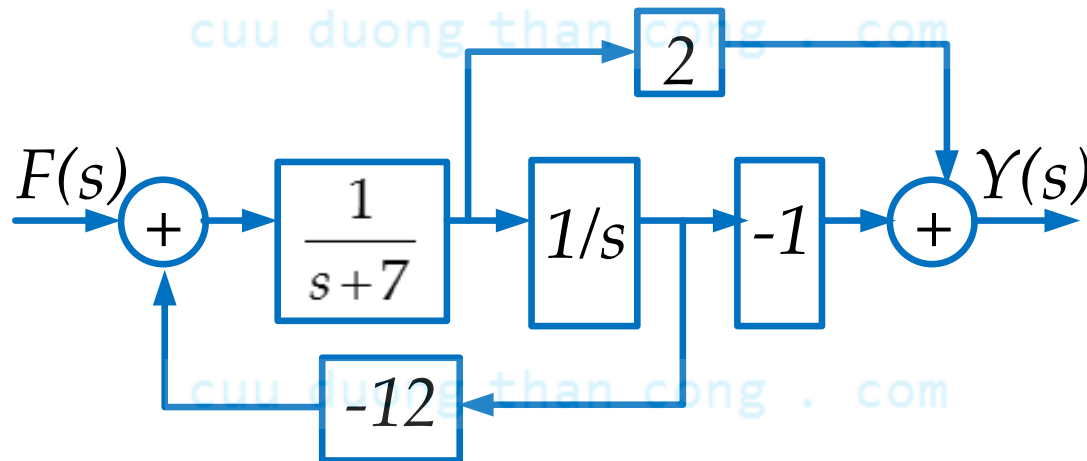


- Feedback: $H(s) = \frac{H_1(s)}{1 + H_1(s)H_2(s)}$



Block diagram:

- Example 5.02:
 - Find transfer function $H(s)$
 - Is that system stable or unstable?
 - Find the output $y(t)$ with the input $f(t) = e^{-2t}u(t)$



Chapter 5:

System analysis using transfer function

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System described by differential equation:

- Systems that are described by a differential equation:

$$a_n y^{(n)}(t) + \dots + a_1 y'(t) + a_0 y(t) = b_m f^{(m)}(t) + \dots + b_1 f'(t) + b_0 f(t)$$

- In this course, we assume $m \leq n$.
- Differential operator $D = d/dt$:

$$(D^n + a_{n-1}D^{n-1} + \dots + a_1D + a_0)y(t) = (b_mD^m + b_{m-1}D^{m-1} + \dots + b_1D + b_0)f(t)$$

$$\Leftrightarrow Q(D)y(t) = P(D)f(t)$$

- Laplace transform (assume that all initial conditions are zero):

$$D^n y(t) \leftrightarrow s^n Y(s)$$

$$D^m f(t) \leftrightarrow s^m F(s)$$

Transfer function and impulse response:

- Laplace transform of system equation:

$$Q(D)y(t) = P(D)f(t)$$
$$\leftrightarrow Q(s)Y(s) = P(s)F(s)$$

- Transfer function:

$$H(s) = \frac{Y(s)}{F(s)} = \frac{P(s)}{Q(s)}$$

- Impulse response:

$$h(t) = \mathcal{L}^{-1}\{H(s)\}$$

- Example 5.03: Find the impulse response of the system
 $(D^3 + 7D^2 + 19D + 13)y(t) = (D - 1)f(t)$

Chapter 5:

System analysis using transfer function

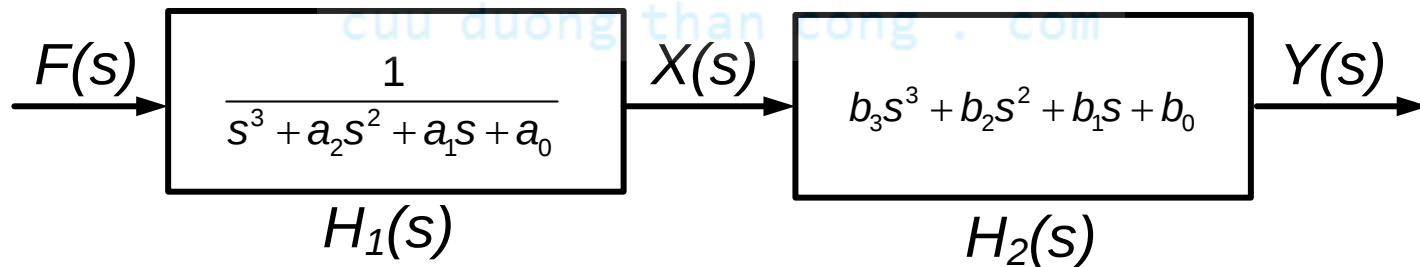
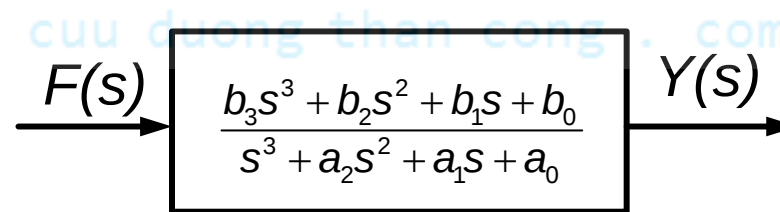
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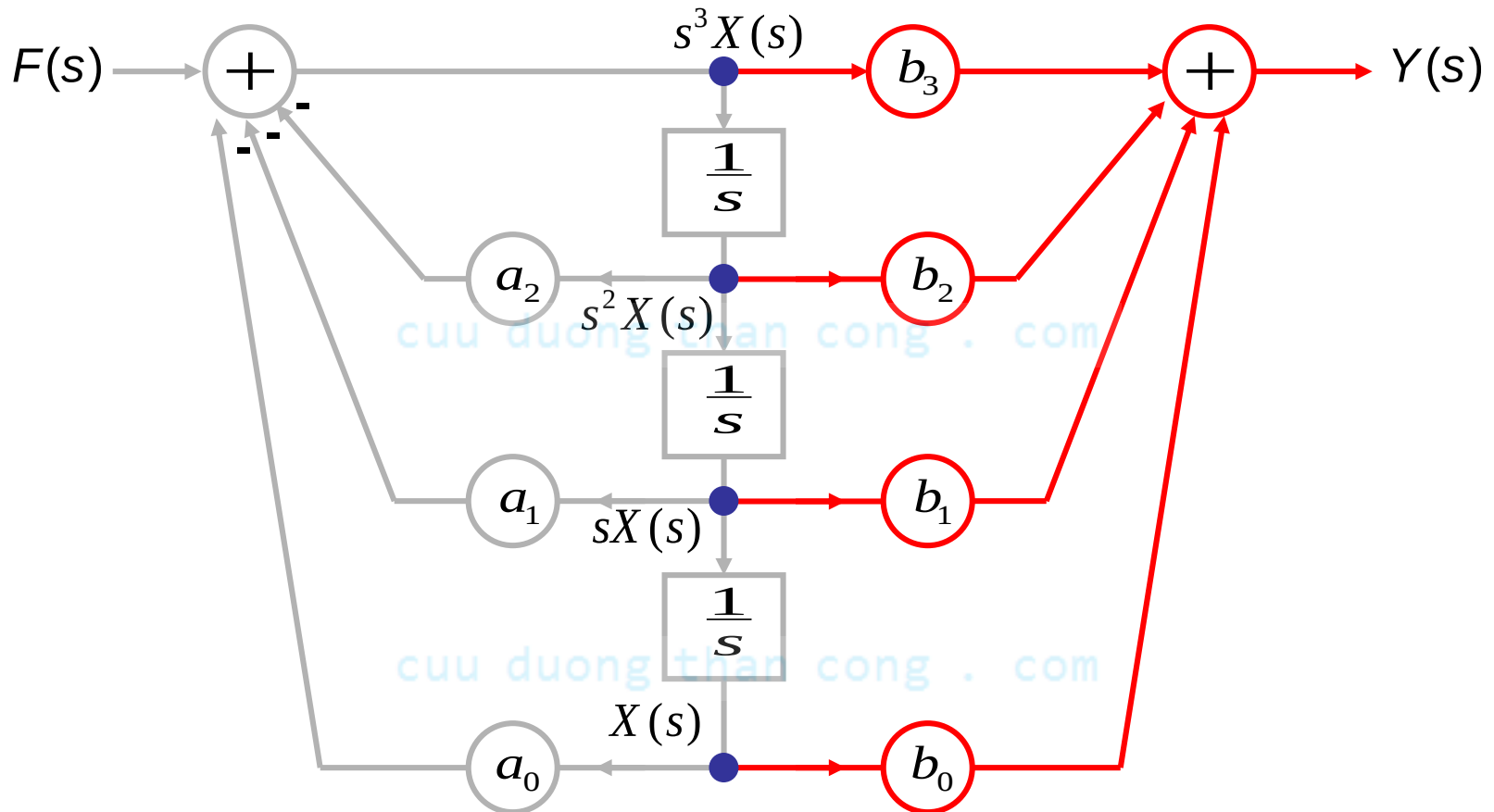
Canonical or Direct-Form Realization:

- For example, we consider a third-order system:

$$H(s) = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{s^3 + a_2 s^2 + a_1 s + a_0}$$



Canonical or Direct-Form Realization:



Canonical or Direct-Form Realization:

- Example 5.04: Find the canonical realization of the following transfer functions:

a. $\frac{5}{s+2}$

b. $\frac{s+5}{s+7}$

c. $\frac{s}{s+7}$

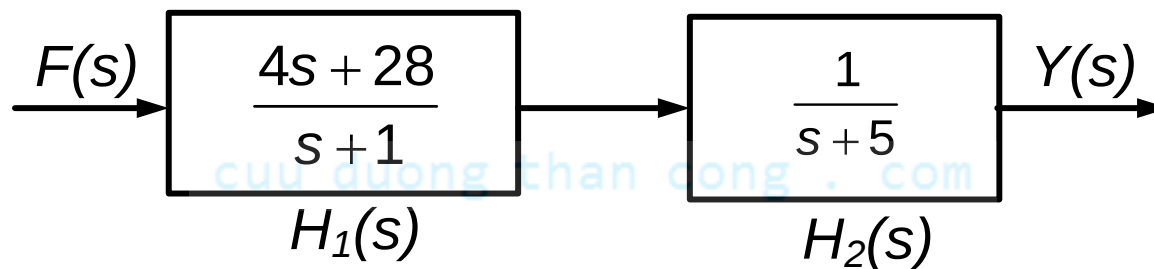
d. $\frac{4s+28}{s^2+6s+5}$

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Cascade realization:

- An n th-order transfer function $H(s)$ can be expressed as a **product** of n first-order transfer functions.

$$H(s) = \frac{4s + 28}{s^2 + 6s + 5} = \underbrace{\left(\frac{4s + 28}{s + 1} \right)}_{H_1(s)} \underbrace{\left(\frac{1}{s + 5} \right)}_{H_2(s)}$$

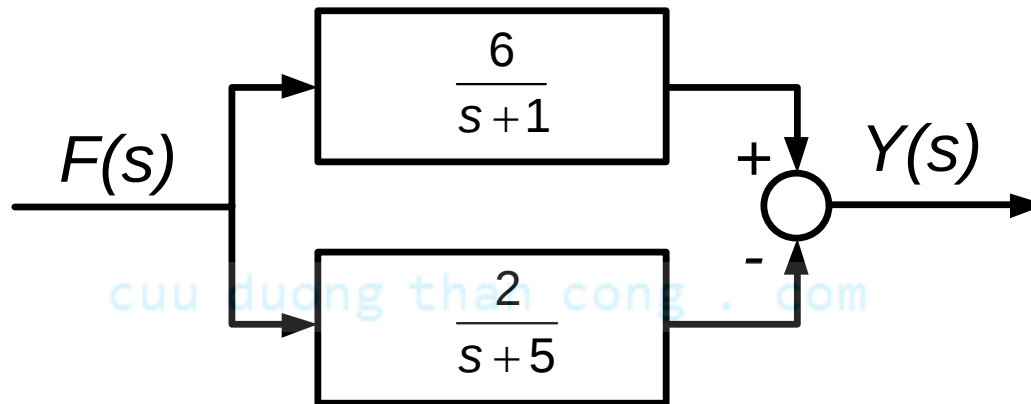


Parallel realization:

- An n th-order transfer function $H(s)$ can be expressed as a **sum** of n first-order transfer functions.

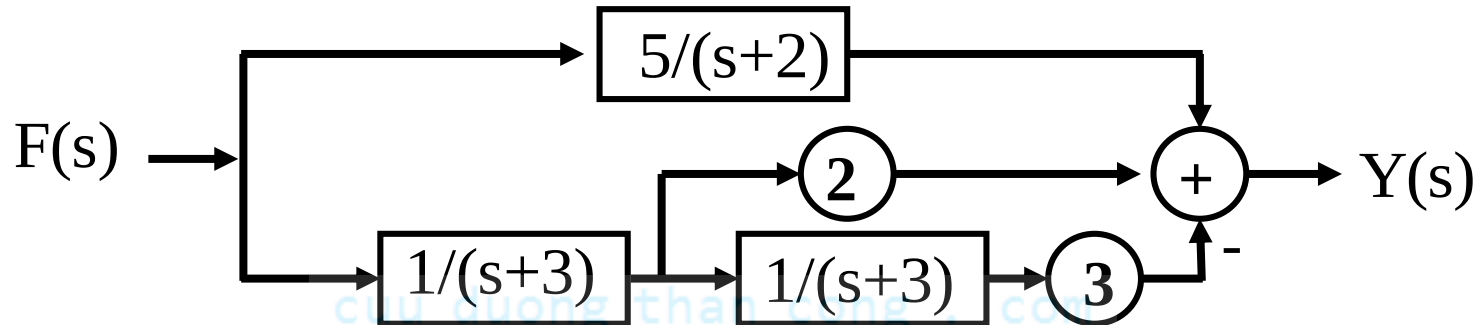
$$H(s) = \frac{4s + 28}{s^2 + 6s + 5} = \frac{6}{s + 1} - \frac{2}{s + 5}$$

$H_3(s)$ $H_4(s)$

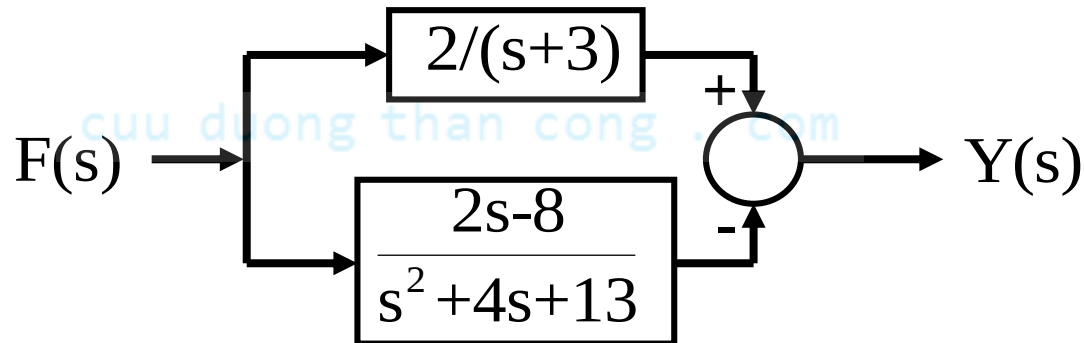


Some special cases:

$$H(s) = \frac{7s^2 + 37s + 51}{(s+2)(s+3)^2} = \frac{5}{s+2} + \frac{2}{s+3} - \frac{3}{(s+3)^2}$$



$$H(s) = \frac{10s + 50}{(s+3)(s^2 + 4s + 13)} = \frac{2}{s+3} - \frac{2s-8}{s^2 + 4s + 13}$$

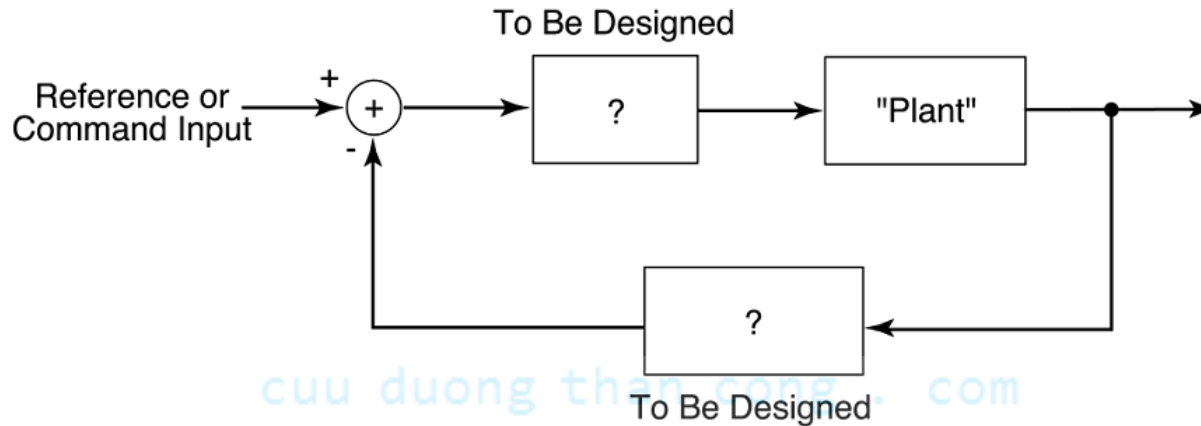


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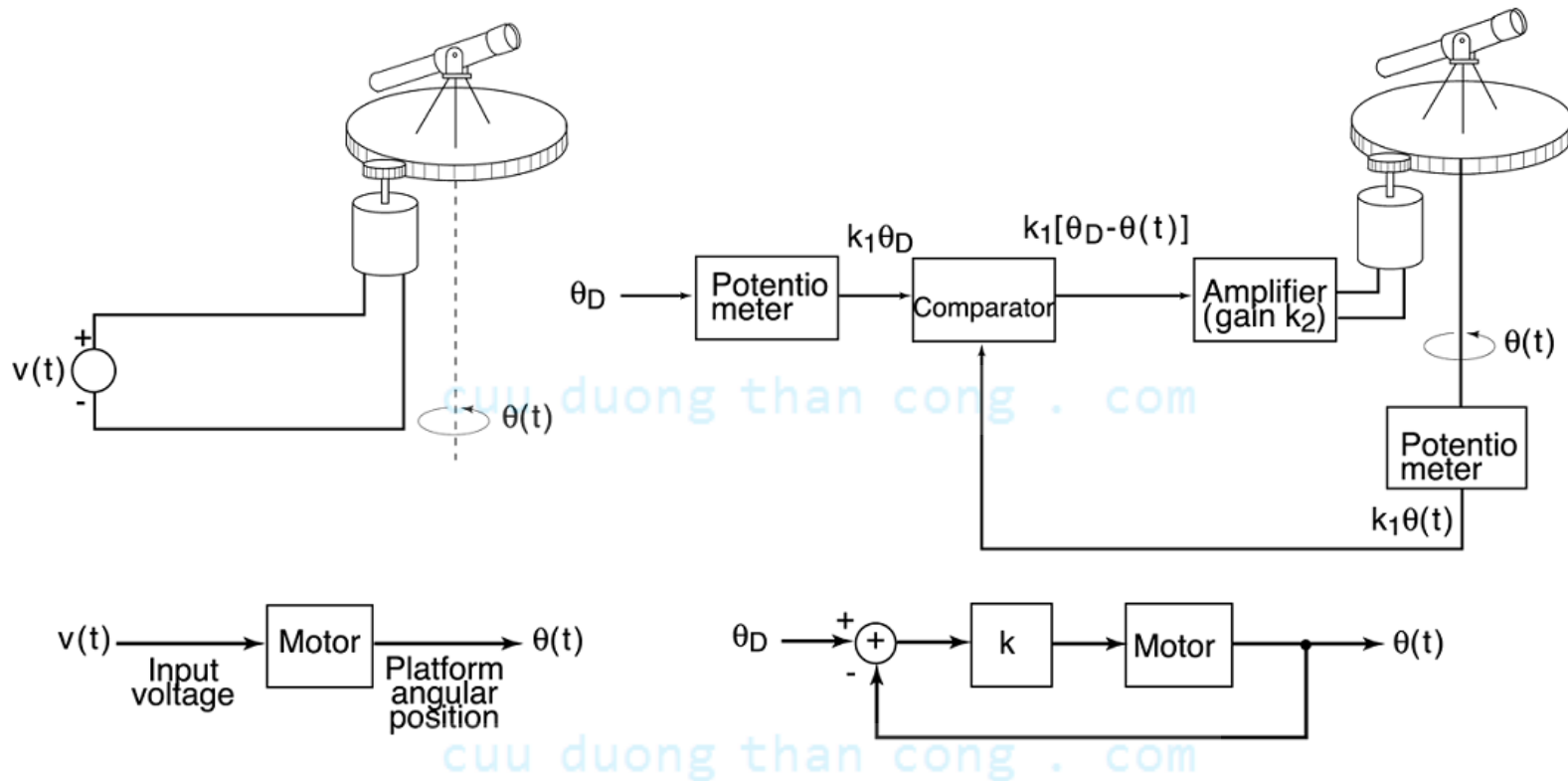
A typical feedback system:



➤ Why use Feedback?

- Reducing Effects of Nonidealities and Disturbances
- Reducing Sensitivity to Uncertainties and Variability
- Stabilizing Unstable Systems
- Tracking

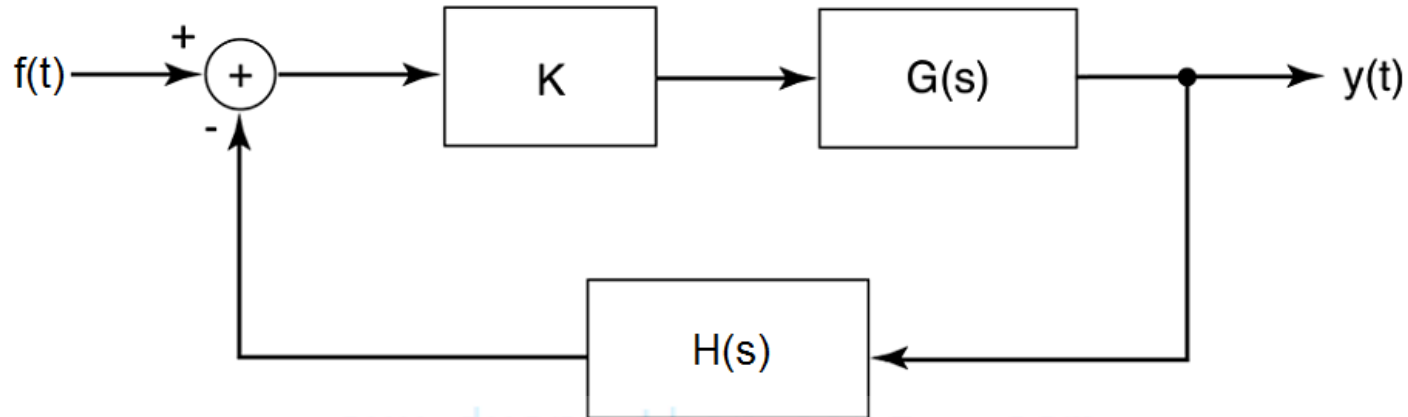
A typical feedback system:



Open-Loop System

Closed-Loop Feedback System

The Use of Feedback to Compensate for Nonidealities



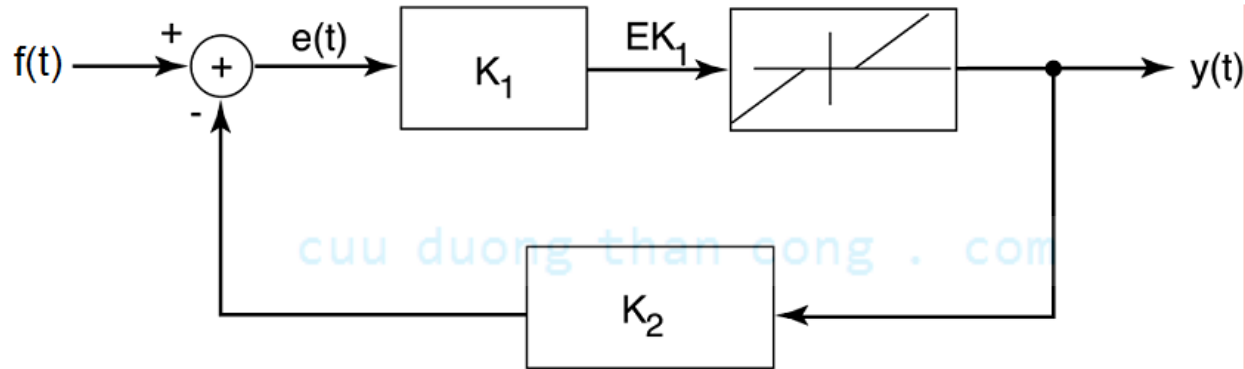
➤ If $|KG(s)H(s)| \gg 1$:

$$T(s) = \frac{Y(s)}{F(s)} = \frac{KG(s)}{1 + KG(s)H(s)} \approx \frac{1}{H(s)}$$

Independent of $G(s)$!!

Compensation for Nonlinearities

- Amplifier with a Dead-zone: cause distortion



- If the loop gain (K_1, K_2) is large enough, the input-output response $\approx 1/K_2$.

Reduced Sensitivity

- Suppose $KG(s) = 1000$, $H(s) = 0.099$

$$T(s) = \frac{1000}{1 + (1000)(0.099)} = 10$$

- Suppose $KG(s) = 500$, $H(s) = 0.099$ (50% gain change)

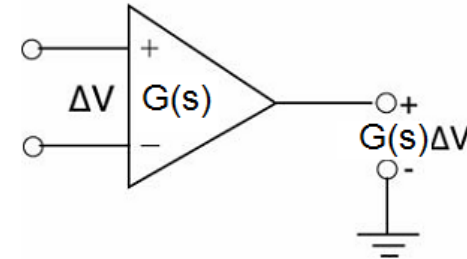
$$T(s) = \frac{500}{1 + (500)(0.099)} \approx 9.9 \quad (1\% \text{ gain change})$$

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Improving the Dynamics of Systems

- Operational Amplifier 741:

$$G(s) = \frac{10^7}{s + 40}$$

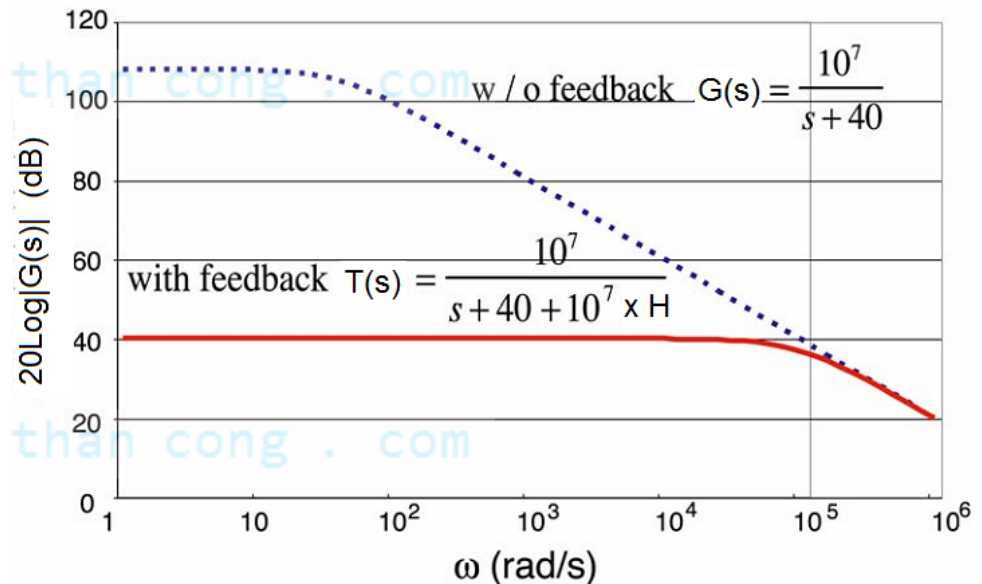


- With feedback:

$$T(s) = \frac{G(s)}{1 + G(s)H(s)}$$

$$= \frac{10^7}{s + 40 + 10^7 H(s)}$$

Much broader bandwidth!



Stabilization of Unstable Systems

- If $G(s)$ is unstable, design $K, H(s)$ so that the closed-loop system is stable

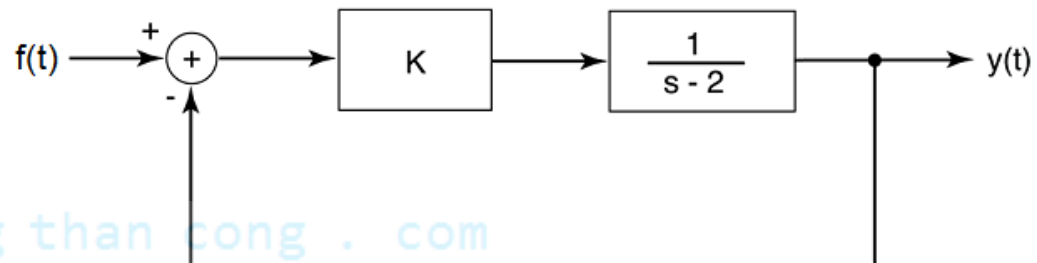
$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)}$$

- **Poles** of $T(s)$ = **roots** of $1 + KG(s)H(s)$ in LHP

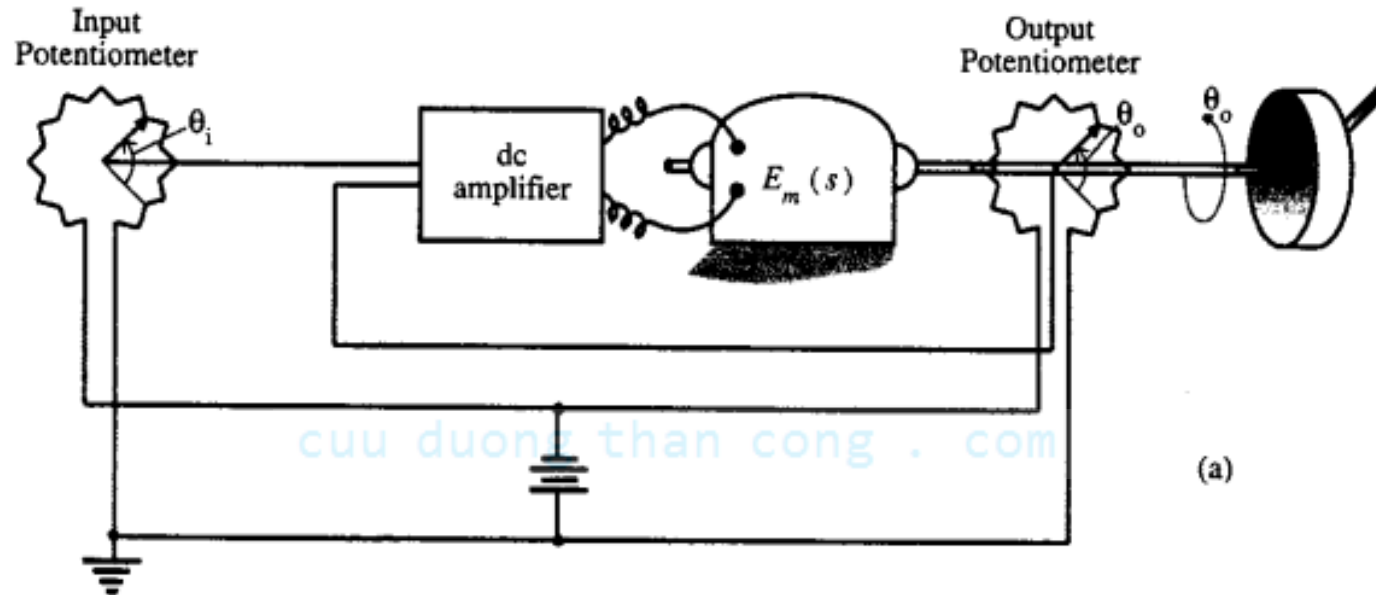
Example:

$$G(s) = \frac{1}{s-2} : \text{unstable}$$

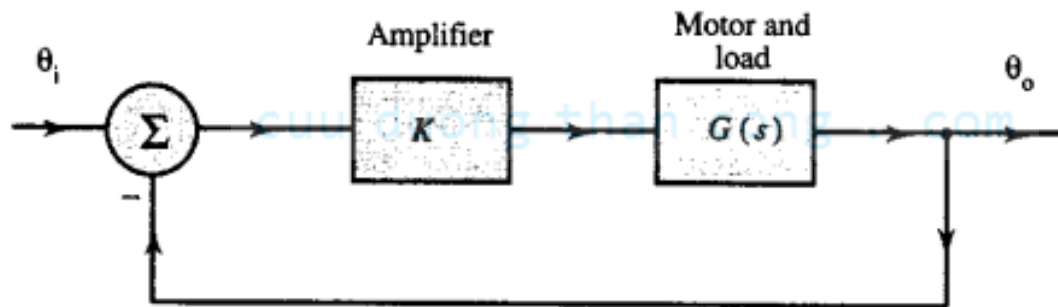
$$T(s) = \frac{K}{s-2+K} : \text{stable as long as } K > 2$$



Analysis of a Simple Control System



(a)



(b)

Analysis of a Simple Control System

- The motor transfer function: $G(s) = \frac{1}{s(s+8)}$
$$\Rightarrow T(s) = \frac{K}{s^2 + 8s + K} \Rightarrow \theta_o(s) = \frac{K}{s^2 + 8s + K} \theta_i(s)$$

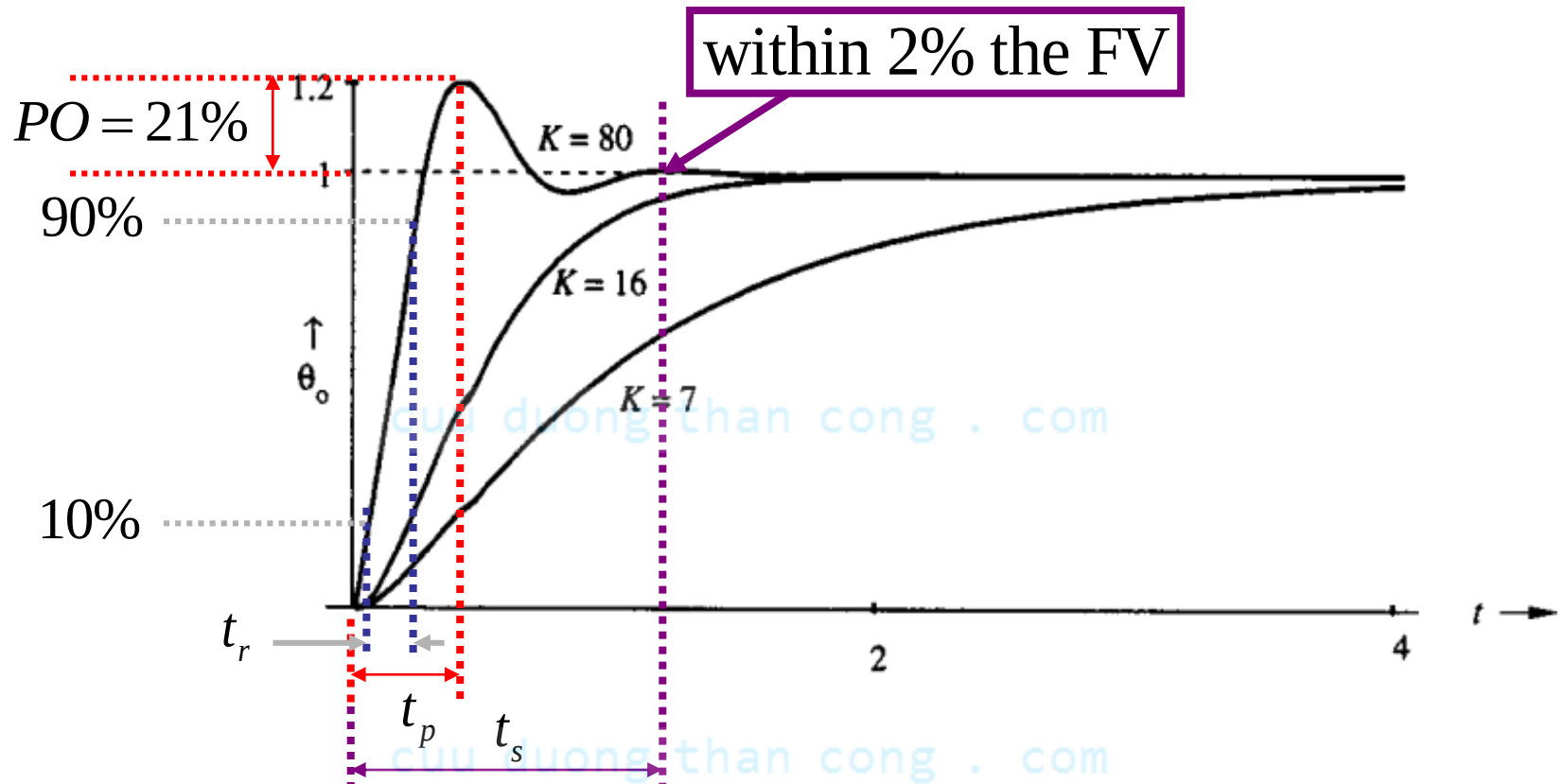
- Step input: $\theta_i(t) = u(t) \Rightarrow \theta_o(s) = \frac{K}{s(s^2 + 8s + K)}$

$$K = 7 \Rightarrow \theta_o(t) = \left(1 - \frac{7}{6}e^{-t} + \frac{1}{6}e^{-7t} \right) u(t) \quad \text{overdamped}$$

$$K = 16 \Rightarrow \theta_o(t) = \left[1 - (4t + 1)e^{-4t} \right] u(t) \quad \text{critically damped}$$

$$K = 80 \Rightarrow \theta_o(t) = \left[1 - \frac{\sqrt{5}}{2}e^{-4t} \cos(8t - 0.4636) \right] u(t) \quad \text{underdamped}$$

Analysis of a Simple Control System



PO : percent overshoot
 t_r : rise time

t_p : peak time
 t_s : settling time

Design Specifications:

1. Transient Response:

- Specified overshoot to step input
- Specified rise time t_r and/or delay time t_d
- Specified settling time t_s

2. Steady-State Error

- Specified steady-state error to certain expected inputs such as step, ramp, or parabolic inputs.
- Notes: $e(t) = f(t) - y(t) \Rightarrow E(s) = F(s) - Y(s) = F(s)[1 - T(s)]$

$$e_{ss} = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} [sE(s)]$$

Steady-State Error:

For the system with unity feedback: $T(s) = \frac{KG(s)}{1 + KG(s)H(s)}$

$$E(s) = \frac{1}{1 + KG(s)} F(s)$$

a. Step input $f(t) = u(t)$:

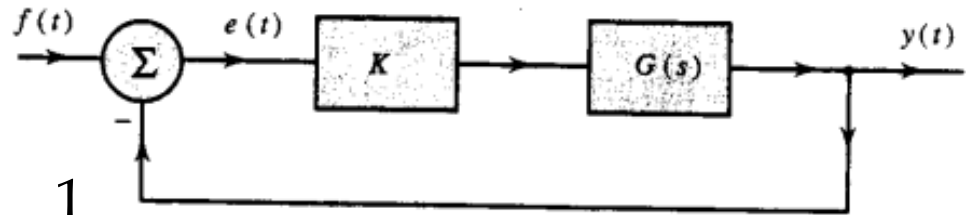
$$e_s = \lim_{s \rightarrow 0} \left[s \frac{1}{1 + KG(s)} \frac{1}{s} \right] = \frac{1}{1 + K_p};$$

$K_p = \lim_{s \rightarrow 0} [KG(s)]$: positional error constant

b. Ramp input $f(t) = tu(t)$:

$$e_r = \lim_{s \rightarrow 0} \left[s \frac{1}{1 + KG(s)} \frac{1}{s^2} \right] = \frac{1}{K_v};$$

$K_v = \lim_{s \rightarrow 0} [sKG(s)]$: velocity error constant



Steady-State Error:

c. Parabolic input $f(t) = t^2 u(t)$:

$$e_s = \lim_{s \rightarrow 0} \left[s \frac{1}{1 + KG(s)} \frac{1}{s^3} \right] = \frac{1}{K_a};$$

$$K_a = \lim_{s \rightarrow 0} [s^2 KG(s)]: \text{acceleration error constant}$$

For example, if

$$G(s) = \frac{1}{s(s+8)} \Rightarrow \begin{cases} K_p = \infty, & e_s = 0 \\ K_v = \frac{K}{8}, & e_r = \frac{8}{K} \\ K_a = 0, & e_p = \infty \end{cases}$$

Such a system can track position of an object with zero error; in tracking an object moving with constant velocity, it yields a constant error; it can not track a constant acceleration object.

Analysis of a Second-Order System

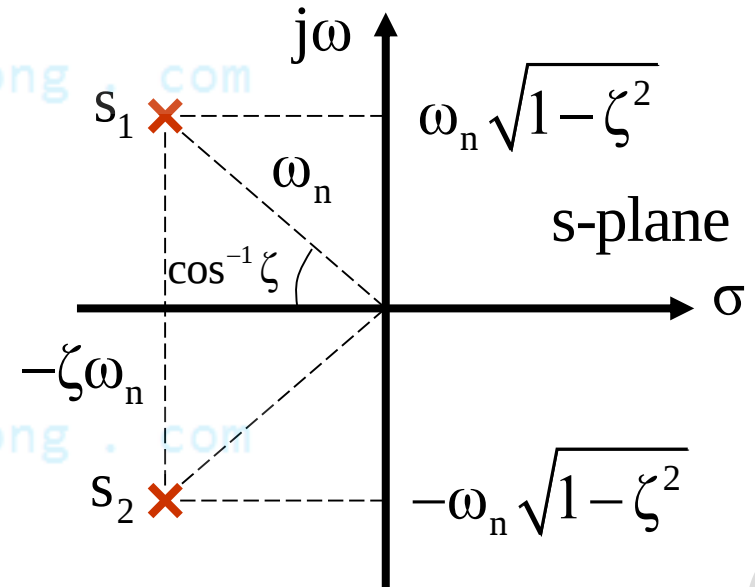
Let's consider a second-order transfer function:

$$T(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}; \quad \zeta - \text{damping ratio}$$

The poles of $T(s)$ are:

$$s_{1,2} = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$

- $\zeta < 1$: underdamped
- $\zeta = 1$: critically damped
- $\zeta > 1$: overdamped

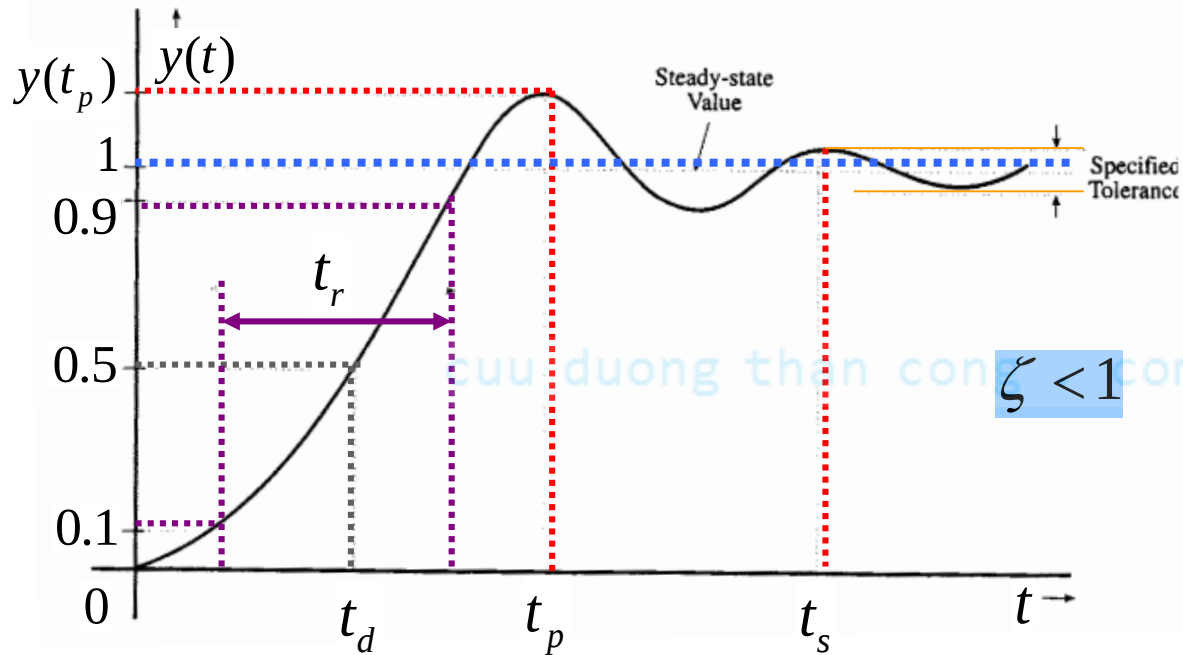


Analysis of a Second-Order System

➤ For the step input $F(s) = 1/s$, the response for the underdamp case ($\zeta < 1$) is:

$$Y(s) = \frac{\omega_n^2}{s(s^2 + 2\zeta\omega_n s + \omega_n^2)} = \frac{1}{s} - \frac{s + 2\zeta\omega_n}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$
$$\Rightarrow y(t) = \left[1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin\left(\omega_n t \sqrt{1-\zeta^2} + \cos^{-1} \zeta\right) \right] u(t)$$

Analysis of a Second-Order System



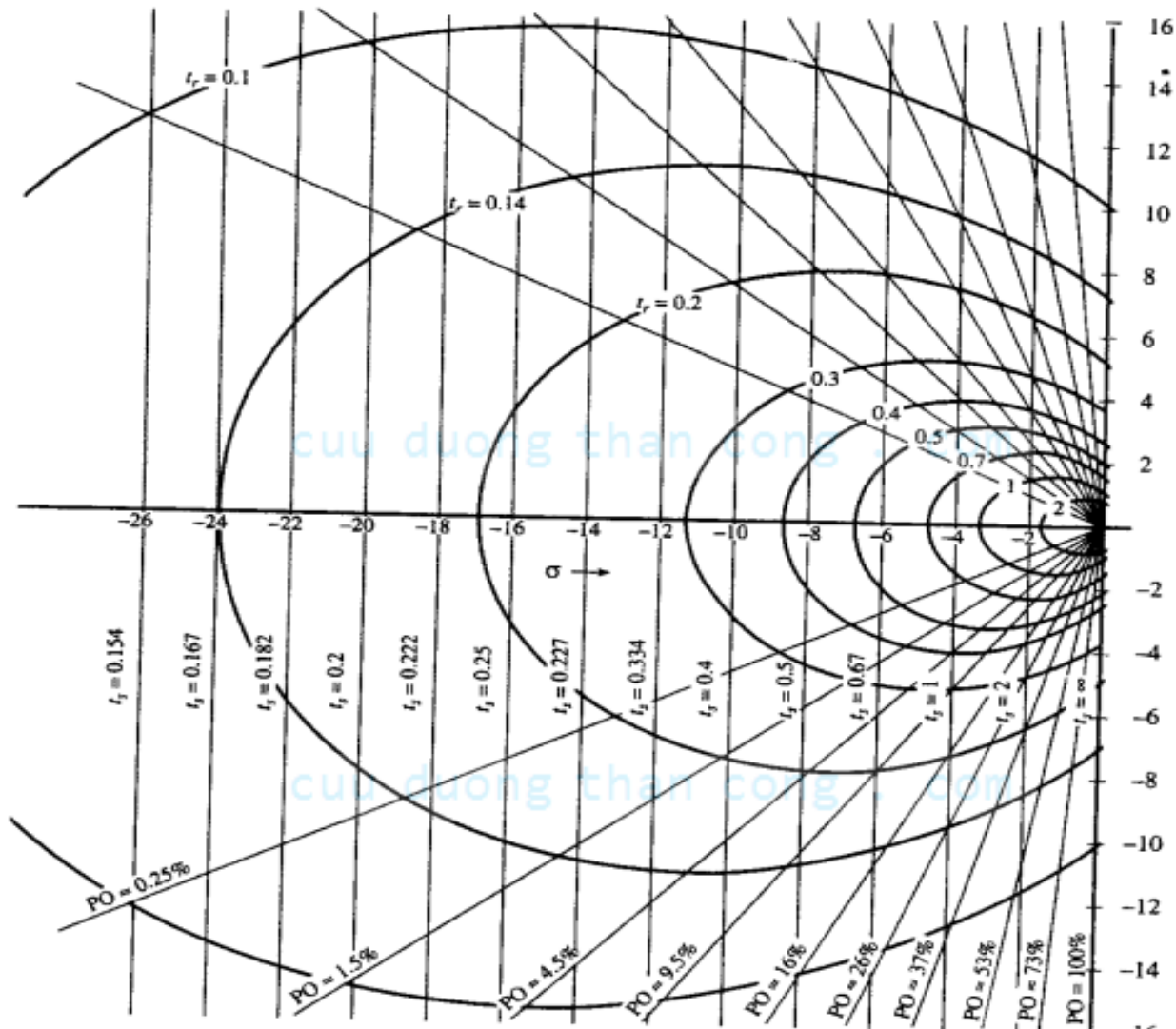
$$t_s = \frac{4}{\zeta \omega_n}$$

$$t_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}}$$

$$PO = 100e^{-\frac{\zeta \pi}{\sqrt{1-\zeta^2}}}$$

$$t_r \approx \frac{1 - 0.4167\zeta + 2.917\zeta^2}{\omega_n}; \quad t_d \approx \frac{1.1 + 0.125\zeta + 0.469\zeta^2}{\omega_n}$$

Analysis of a Second-Order System



Analysis of a Second-Order System

- For example, let the transient specifications for the system

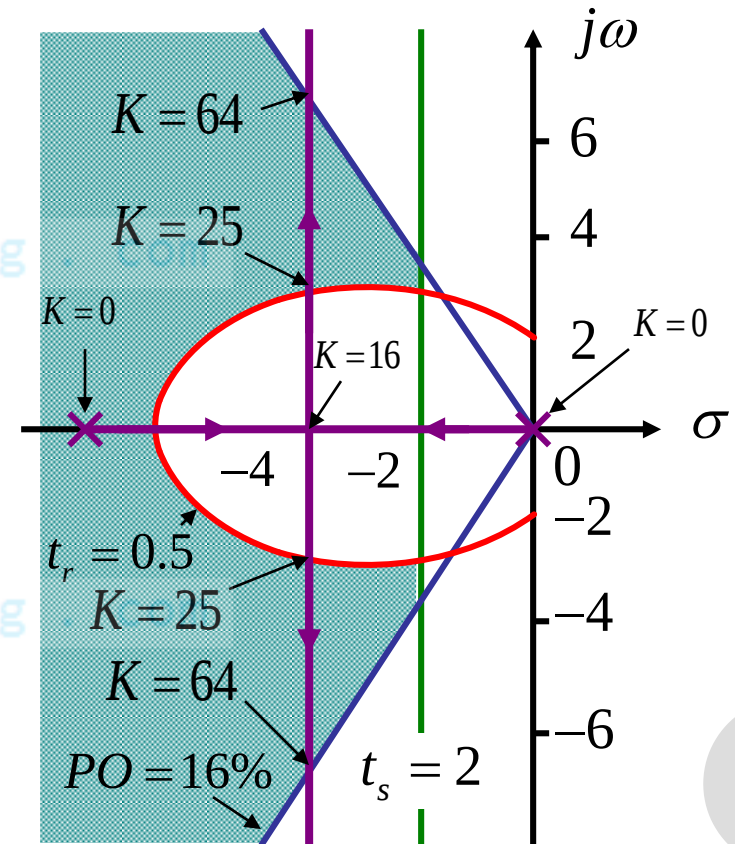
$$T(s) = \frac{K}{s^2 + 8s + K}$$

is $PO < 16\%$, $t_r < 0.5s$, $t_s < 2s$.

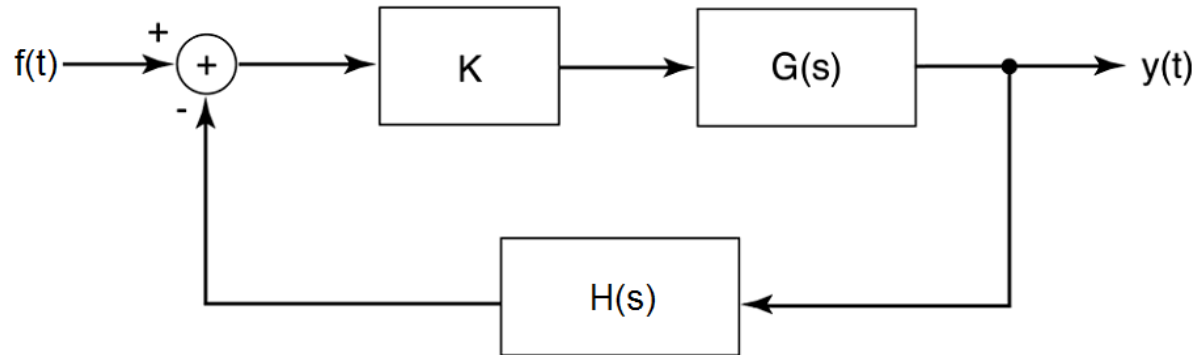
- Poles:

$$s_{1,2} = -4 \pm \sqrt{16 - K}$$

- System will meet the given specifications for $25 \leq K \leq 64$.



Root locus



$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)}$$

- We shall consider the paths of the roots of $1 + KG(s)H(s) = 0$ as K varies from 0 to ∞ .

Rules for Plotting Root Locus

$$G(s)H(s) = -\frac{1}{K}$$

➤ End points:

- At $K = 0$, $G(s_0)H(s_0) = \infty \Rightarrow s_0$ are **poles** of $G(s)H(s)$.
- At $K = \infty$, $G(s_0)H(s_0) = 0 \Rightarrow s_0$ are **zeros** of $G(s)H(s)$.

➤ **Rule #1:**

A root locus starts (at $K = 0$) from a pole of $G(s)H(s)$ and ends (at $K = \infty$) at a zero of $G(s)H(s)$ or at $\pm\infty$.

Notes: in s-plane, the poles are denoted as **x**, the zeros are denote as **o**.

If $G(s)H(s)$ has n **poles** p_i and m **zeros** z_i , m loci terminate on the zeros, the other $n - m$ loci terminate at ∞ .

Rules for Plotting Root Locus

➤ Rule #2:

A real axis segment is a part of the root locus if the sum of the poles and zeros of $G(s)H(s)$ that lie to the right of the segment is odd.

The root locus are symmetric about real axis.

➤ Rule #3:

The centroid of the asymptotes of $(n - m)$ loci that terminate at ∞ is:

$$s = \sigma = \frac{\sum p_i - \sum z_i}{n - m}$$

at the angles:

$$\phi = \frac{(2k + 1)\pi}{n - m}$$

Rules for Plotting Root Locus

➤ Rule #4:

Real axis break-in and break away points:

For each $s = \sigma$ on a real-axis segment of the root locus:

$$KG(\sigma)H(\sigma) = -1 \Rightarrow K = -\frac{1}{G(\sigma)H(\sigma)}$$

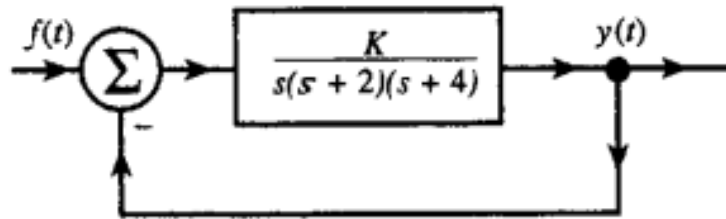
Real axis break-in & breakaway points are the real values of σ for which:

$$\frac{dK(\sigma)}{d\sigma} = 0$$

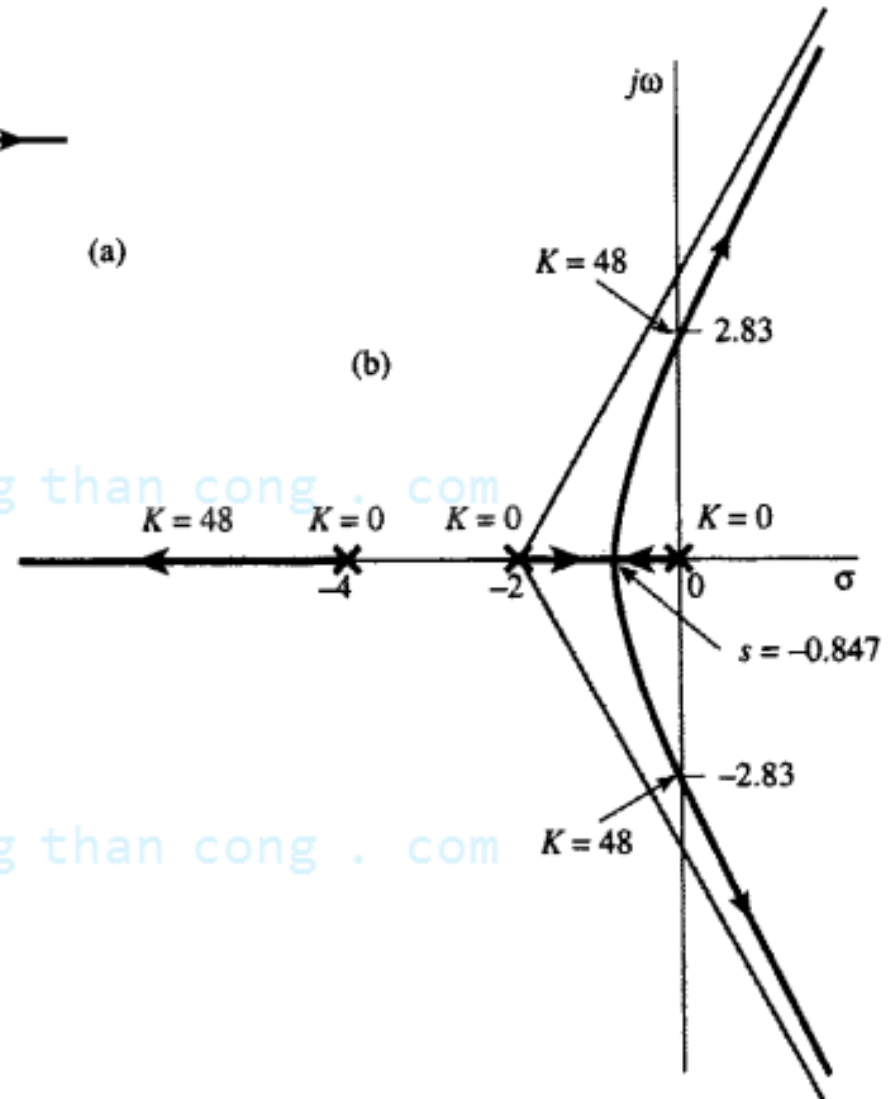
Example: Sketch the root locus for a system with:

$$KG(s)H(s) = \frac{K}{s(s+2)(s+4)}$$

Rules for Plotting Root Locus



(a)



(b)

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